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CERTIFICATION

I, the below named translator, hereby declare that: my name and post office address are as stated below; that I am knowledgeable in the English and German languages, and that I believe that the attached text is a true and complete translation of PCT/DE2004/002455, filed with the German Patent Office on November 2, 2004.

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

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1 Description

2

3 Switching device

4

5 The invention relates to a switching device having a first  
6 and a second arcing contact piece, which lie axially  
7 opposite one another, and a first and a second rated current  
8 contact piece, which are arranged coaxially with respect to  
9 the arcing contact pieces, at least one of the rated current  
10 contact pieces having a hollow-cylindrical basic body, which  
11 is covered at the front by an arc-resistant material at its  
12 end facing a switching path of the switching device.

13

14 Such a switching device has been disclosed, for example, in  
15 the European patent application EP 0 982 748 A1. Therein,  
16 the arcing contact pieces are covered by an arc-resistant  
17 material by means of plasma spraying such that an arc drawn  
18 between the arcing contact pieces does not cause any  
19 erosion, or only causes a very low amount of erosion.  
20 Furthermore, the rated current contact pieces likewise have  
21 an erosion-resistant protective coating, which is applied by  
22 means of plasma spraying, in sections on their sliding  
23 faces. The stationary rated current contact piece is silver-  
24 plated on top of the erosion-resistant protective coating.

25

26 When two or more materials, such as the erosion-resistant  
27 material, the electrically conductive silver and a further  
28 metal such as the aluminum of the rated current contact  
29 piece, impact against one another, the respective points of  
30 impact always have irregularities. The point of impact can  
31 only be subjected to a mechanical load to a reduced extent.  
32 Surface friction occurring in the event of the sliding faces  
33 of the rated current contact pieces running against one  
34 another can result in disintegration phenomena and thus in a  
35 weakening of the individual layers. It is thus possible for

1 individual layers to be chipped off starting from the point  
2 of impact. This reduces the switching capacity of the  
3 switching device.

4

5 The invention is based on the object of designing a  
6 switching device of the type mentioned initially such that  
7 the contact points withstand high mechanical and thermal  
8 loads while having a high current-carrying capacity.

9

10 The object is achieved according to the invention in the  
11 case of the switching device of the type mentioned initially  
12 by the fact that the arc-resistant material has an  
13 electroplating.

14

15 The electroplating may consist, for example, of an  
16 electrically highly conductive material, such as silver or  
17 gold. This reduces the contact resistance of the electrical  
18 contact. At the same time, the electroplating prevents  
19 oxidation on the arc-resistant material in the event that  
20 the individual components are stored for a relatively long  
21 period of time. By including the arc-resistant material in  
22 an electroplating treatment process, it is possible to cover  
23 points of impact or boundary layers of different materials,  
24 which improves the mechanical loadability and the mechanical  
25 endurance of these points.

26

27 One advantageous refinement can furthermore provide for the  
28 arc-resistant material to be fixed to the hollow-cylindrical  
29 basic body in the form of a ring, so as to cover front faces  
30 of the hollow-cylindrical basic body.

31 Owing to the fact that the front faces of the hollow-  
32 cylindrical basic body are covered, the electric field in  
33 the direction of the switching path of the switching device  
34 is substantially controlled by the form of the ring. This  
35 results in the possibility of using manufacturing methods

1 for manufacturing the basic body with a lesser degree of  
2 precision, for example a reduced surface quality, than in  
3 the case of the ring used for field control. Furthermore, it  
4 is possible to equip the basic body with various ring forms  
5 so as to achieve various electric field effects in the  
6 region of the switching path of the switching device.

7 Furthermore, when the front faces of the hollow-cylindrical  
8 basic body are completely covered, the basic body itself is  
9 protected against the effect of a switching arc. It is thus  
10 possible for an arc to act on many points on the ring. The  
11 stability of the ring is thus increased. Splitting into a  
12 hollow-cylindrical basic body and a ring also furthermore  
13 has the advantage that the hollow-cylindrical basic body can  
14 be produced, for example, from a material having a low  
15 density, such as aluminum, as a result of which the total  
16 mass of the hollow-cylindrical basic body and the arc-  
17 resistant material fixed thereto is reduced. Arc-resistant  
18 materials are, for example, mixtures of molybdenum (Mo),  
19 tungsten (W), copper (Cu) and silver (Ag). For example,  
20 CuCrZr, CuZn39Pb3 or Ecu57 can be used for the arc-resistant  
21 material. These materials have a very high density, which  
22 results in the ring having a comparatively high mass. In  
23 particular in the event of a movement of the rated current  
24 contact piece equipped with the arc-resistant material, the  
25 multi-part design of the rated current contact piece limits  
26 the mass to be moved.

27  
28 Provision may advantageously further be made for the ring to  
29 have a smaller radial wall thickness at its end facing away  
30 from the switching path than at its end facing the switching  
31 path.

32  
33 Owing to the high density which has already been mentioned  
34 above, even small components consisting of an arc-resistant  
35 material have a comparatively high mass. A reduction in the

1 wall thicknesses to the absolute minimum required therefore  
2 makes it possible to make savings on the arc-resistant  
3 material. Furthermore, in the case of a stepped design of  
4 the ring, in which the end facing the switching path has a  
5 greater wall thickness than the end facing away from the  
6 switching path, it is possible for the ring to be pushed  
7 onto the hollow-cylindrical basic body in a simple manner.  
8 Owing to this design for the form of the ring, it can be  
9 pushed onto the hollow-cylindrical basic body automatically  
10 in a centering manner. This simplifies assembly. At the same  
11 time, the points of the hollow-cylindrical basic body and  
12 the arc-resistant ring which are coming into contact with  
13 one another are increased in number owing to the enlarged  
14 area. Owing to an increased number of contact points, the  
15 electrical contact resistance between the arc-resistant ring  
16 and the hollow-cylindrical basic body is reduced.

17  
18 One further advantageous refinement may provide for the ring  
19 to be pressed against the hollow-cylindrical basic body of  
20 the rated current contact piece in the axial direction by  
21 means of a bolt connection.

22  
23 A bolt connection in the axial direction between the ring  
24 and the hollow-cylindrical basic body makes it possible to  
25 keep the outer contours of the ring and the hollow-  
26 cylindrical basic body free from drilled holes or other  
27 fixing means. The outer contour of the rated current contact  
28 piece is thus maintained. Furthermore, owing to an  
29 arrangement of the bolt connections in the axial direction  
30 in the interior of the hollow-cylindrical basic body, a  
31 sufficient volume remains free for accommodating, for  
32 example, further assemblies or for deflecting or guiding the  
33 quenching gas flows occurring in the event of a switching  
34 operation in the interior. Threaded rods, screws, pressed or  
35 crimped bolts or bolts which have been adhesively bonded-in

1 etc. can be used for bolting purposes. In this case, the  
2 bolts form a type of cage with their longitudinal axes  
3 parallel to the cylinder axis of the hollow-cylindrical  
4 basic body. Owing to an even distribution over the  
5 circumference of the hollow-cylindrical basic body, the ring  
6 can be pressed uniformly against the hollow-cylindrical  
7 basic body.

8  
9 One further advantageous refinement may provide for the  
10 hollow-cylindrical basic body to have a radial projection,  
11 against which an insulating body, in particular an  
12 insulating material nozzle, is pressed axially by means of a  
13 pressure element.

14  
15 The radial projection represents a fixed stop for the  
16 insulating body. The position of the insulating body with  
17 respect to the hollow-cylindrical basic body is thus clearly  
18 fixed. The incorporation of the insulating body takes place  
19 by means of a pressure element over a short period of time.  
20 Additional measurements, adaptations or adjustments of the  
21 insulating body are thus not required. An annular disk,  
22 which transfers the contact-pressure force evenly over the  
23 insulating body, can be used, for example, as the pressure  
24 element. In this case, it is advantageous if the radial  
25 projection is likewise designed to be annular and  
26 circumferential.

27  
28 Provision may advantageously also be made for the hollow-  
29 cylindrical basic body to have a reduced outer diameter at  
30 its end facing the switching path and for the radial  
31 projection to be arranged on the hollow-cylinder inner  
32 casing in the region of the reduced outer diameter.

33  
34 With such an arrangement of the radial projection, a  
35 sufficient distance is produced between the contact-pressure



1 cheeks of the projection and the pressure element to make  
2 advantageous use of the intrinsic elasticity of the  
3 insulating body material. Owing to thermal influences,  
4 expansions or shrinkages of the insulating material result.  
5 It is therefore necessary when using a clamping connection  
6 to cover a sufficient insulating body volume. Only in this  
7 manner is it possible for sufficient holding force to act on  
8 the insulating body in the case of various thermal loads. A  
9 clamping region which is too small would not be suitable for  
10 permanently applying the required forces. Furthermore, the  
11 insulating body can be stopped very close to the front of  
12 the hollow-cylindrical basic body. The required physical  
13 length for the total construction of fixing the erosion-  
14 resistant ring and the insulating material nozzle to the  
15 hollow-cylindrical basic body is thus reduced.

16  
17 A further advantageous refinement may provide for the ring  
18 to have fixing devices in the region of its enlarged radial  
19 wall thickness.

20  
21 Sections having an enlarged wall thickness make it possible  
22 to flexibly select the location of fixing devices. At the  
23 same time, such sections have a comparatively high  
24 mechanical strength. For example, threaded holes or other  
25 anchoring points may be provided as the fixing devices.

26  
27 Provision may advantageously be made for contact-making  
28 points between the two rated current contact pieces to lie  
29 axially in the region of the arc-resistant material in the  
30 switched-on state of the switching device.

31  
32 An arrangement of the contact-making points of the two rated  
33 current contact pieces in the region of the arc-resistant  
34 material prevents, from the outset, a situation in which the  
35 individual contact faces need to be moved over joints during

1 a switching operation. As a result, the joints are protected  
2 against mechanical loading resulting from the corresponding  
3 contact parts of the rated current contact pieces being  
4 pushed on and pushed away. For this reason it is possible to  
5 manufacture the joints with increased tolerance. It is  
6 barely possible for an electroplating to be removed at this  
7 joint owing to mechanical loading of the rated current  
8 contact pieces. The robustness of the contact pieces of the  
9 switching device is thus improved.

10

11 The invention will be shown schematically in a drawing and  
12 described in more detail below with reference to an  
13 exemplary embodiment.

14

15 In the drawing

16

17 Figure 1 shows a section through a switching device,

18

19 Figure 2 shows a further section through the switching  
20 device, and

21

22 Figure 3 shows a section through the switching device shown  
23 in figures 1 and 2, along the axis A-A.

24

25 The switching device illustrated in figure 1 is a high-  
26 voltage power breaker 1. A high-voltage power breaker 1 is  
27 used to switch rated currents and short-circuit currents.  
28 The high-voltage power breaker 1 has a first arcing contact  
29 piece 2 and a second arcing contact piece 3. The first  
30 arcing contact piece 2 is essentially cylindrical and has a  
31 coating of an arc-resistant material at its end facing the  
32 switching path of the high-voltage power breaker 1. The  
33 second arcing contact piece 3 is in the form of a tulip  
34 contact, in which the first arcing contact piece 2 can be  
35 inserted. At its end facing the switching path, the second



1 arcing contact piece 3 likewise has a coating of arc-  
2 resistant material. The two arcing contact pieces 2, 3 are  
3 arranged axially opposite one another on a main axis 4. A  
4 first rated current contact piece 5 is arranged  
5 concentrically with respect to the first arcing contact  
6 piece 2. A second rated current contact piece 6 is arranged  
7 concentrically with respect to the second arcing contact  
8 piece 3. The first rated current contact piece 5 has a large  
9 number of elastic contact fingers 7 at its end facing the  
10 switching path, said contact fingers 7 being in electrically  
11 conductive contact with the outer casing of the second rated  
12 current contact piece 6 in the closed state of the high-  
13 voltage power breaker 1. Furthermore, the second arcing  
14 contact piece 3 is surrounded by an insulating material  
15 nozzle 8. The insulating material nozzle 8 is held on the  
16 second rated current contact piece 6. The rated current  
17 contact pieces 5, 6 and the arcing contact pieces 2, 3 can  
18 be moved in relation to one another along the main axis 4,  
19 to be precise such that, in the case of a switch-on  
20 operation, initially the arcing contact pieces 2, 3 and then  
21 the rated current contact pieces 5, 6 come into contact with  
22 one another. In the event of a switch-off operation,  
23 initially the rated current contacts 5, 6 open, and then the  
24 arcing contact pieces 2, 3 are isolated from one another.  
25 The second rated current contact piece 6 has an essentially  
26 hollow-cylindrical basic body 6a. The hollow-cylindrical  
27 basic body 6a is covered at the front by a ring 9 of an arc-  
28 resistant material. The ring likewise has an essentially  
29 hollow-cylindrical structure, the hollow cylinder top face,  
30 which faces the switching path of the high-voltage power  
31 breaker 1, being rounded off. Furthermore, the wall  
32 thickness of the ring 9 on the side facing away from the  
33 switching path is less than on its side facing the switching  
34 path. In the present exemplary embodiment, this is achieved  
35 by the inner diameter of the ring 9 being enlarged on its

1 side facing away from the switching path. Furthermore, a  
2 conical or parabolic profile of the inner casing surface of  
3 the ring 9 or other suitable geometric shapes can also be  
4 used. The hollow-cylindrical basic body 6a has a reduced  
5 outer diameter at its end facing the switching path. The  
6 reduced outer diameter of the hollow-cylindrical basic  
7 body 6a and the enlarged inner diameter of the ring 9 are  
8 matched to one another such that the ring 9 can be pushed  
9 onto the hollow-cylindrical basic body 6a. In order to press  
10 the ring 9 against the hollow-cylindrical basic body 6a, the  
11 ring 9 has a plurality of threaded holes, into which bolts  
12 10 can be screwed. The bolts 10 are supported in each case  
13 at edges of cutouts, which are arranged distributed  
14 symmetrically, parallel to the main axis 4, in the casing of  
15 the hollow-cylindrical basic body 6a. The surface of the  
16 ring 9 is electroplated. This electroplating is, for  
17 example, a silver plating. The hollow-cylindrical basic  
18 body 6a is likewise provided with an electroplating. In the  
19 switched-on state of the high-voltage power breaker 1, the  
20 contact points of the electrical contact fingers 7 rest in  
21 the region 11 of the ring 9. Owing to the arrangement of the  
22 ring 9 of an arc-resistant material, high switching powers  
23 can also be controlled, in the case of which switching arcs  
24 occur, despite the use of arcing contact pieces, even on the  
25 rated current contact pieces. The use of the arc-resistant  
26 ring 9 allows for a compact design of a high-voltage power  
27 breaker.

28  
29 Figure 2 illustrates a section through the high-voltage  
30 power breaker 1 known from figure 1. However, the sectional  
31 plane is pivoted about the main axis 4 such that it is now  
32 possible to see the fixing of the insulating material nozzle  
33 8. The insulating material nozzle 8 is held by means of  
34 further bolts 11, which can be screwed into threaded holes  
35 in the essentially hollow-cylindrical basic body 6a. In this

1 case, the threaded holes are aligned such that the further  
2 bolts 11, just like the bolts 10, are arranged parallel to  
3 the main axis 4. The hollow-cylindrical basic body 6a has an  
4 annular projection 12. A circumferential shoulder of the  
5 insulating material nozzle 8 is pressed against the annular  
6 projection 12. The contact-pressure force of the shoulder  
7 against the annular projection 12 is produced by means of a  
8 pressure element 13 in the form of a pressure disk, which is  
9 held by the further bolts 11. The annular projection 12 is  
10 arranged on the inner casing side of the essentially hollow-  
11 cylindrical basic body 6a, to be precise in the section 14  
12 in which the outer diameter of the hollow-cylindrical basic  
13 body 6a is reduced.

14  
15 Figure 3 shows a section along the sectional plane A-A  
16 illustrated in figures 1 and 2. The pressure element 13 has  
17 a structure which is in the form of an annular disk and  
18 which has cutouts, through which the further bolts 11 pass.  
19 The pressure element 13 is pressed against the projection 12  
20 by means of the further bolts 11, with the interposition of  
21 the projecting shoulder of the insulating material nozzle 8.  
22 Furthermore, the pressure element 13 is designed such that,  
23 in order to achieve a small total diameter for the  
24 arrangement, the pressure element 13 has lateral notches in  
25 order to make it possible to fix the ring 9 by means of the  
26 bolts 10. This design makes it possible to fix the ring 9 or  
27 the insulating material nozzle 8 independently of one  
28 another. As a result, the two connections are decoupled from  
29 one another. Any interference or thermal expansions etc. at  
30 one connection point are thus largely kept away from the  
31 other connection.

32

33